

## FUEL CELL SYSTEM POWER CONTROL METHOD AND SYSTEM

## FIELD OF THE INVENTION

The present invention relates generally to the field of power generation, and  
5 more particularly to an improved fuel cell-based power conversion system.

## BACKGROUND OF THE INVENTION

Figure 1 shows a block diagram of a power conversion system that can be  
used with a fuel cell stack 10. Since the fuel source normally cannot keep up with  
10 load transients, it is often necessary to include, in addition to a power conditioner  
12A, a battery 14 or other energy storage device to provide power during load  
transients. Figure 1 shows a switch  $S_1$  used to disconnect the fuel cell stack from the  
system. Switch  $S_1$  may also be used to prevent reverse flow of current into the stack.  
Power conditioner 12A processes the power from the fuel cell stack 10 to a common  
15 dc bus 16. Power conditioner 12A must operate over a large range of input voltage  
since the fuel cell stack voltage changes significantly with load. A second power  
conditioner 12B controls the flow of power between the battery 14 (or other storage  
element) and the dc bus 16. A load 18 and an auxiliary power requirement 20 are also  
shown in Figure 1.

20 The fuel cell system balance of plant (BOP) requires auxiliary power 20 to  
operate. The BOP may comprise blowers, pumps, or sensors. The auxiliary power 20  
would normally be drawn from a relatively constant voltage source to reduce the cost  
of the BOP components. It would therefore be standard practice to draw the auxiliary  
power either directly from the battery 14 or from the common dc bus 16. Since the  
25 BOP components ultimately derive their power from the fuel cell stack, the system  
efficiency would be higher if the BOP components were connected to the common dc  
bus rather than to the battery. (I.e. – it saves the extra power loss that would occur in  
power conditioner 12B to connect the BOP components to the common dc bus rather  
than to the battery.)

30 Figure 2 depicts a specific example of the system illustrated in Figure 1. The  
system shown in Figure 2 could be used as a telecommunications power supply. In  
this example, the load 18 comprises a 48V battery (not shown) in parallel with  
electronic loads, and so the output of the fuel cell system should be maintained at the  
float voltage of the battery, approximately 55V for a nominally 48V battery. In this

specific example, a first power conditioner 12A' could be a dc-to-dc converter (or boost converter when it is used to boost the fuel cell voltage) for providing a dc voltage to the dc bus. A second power converter 12B' would have to allow the power to flow in both directions to permit the battery 14' to provide power to the load 18 as well as to be recharged from the fuel cell stack 10'.

Figure 2 also shows the maximum power-output or power-handling capability of each system component. The auxiliary load 20' is assumed to be a maximum of 400W and the telecommunications load 18 is assumed to be 1kW maximum. The fuel cell stack 10' should be able to provide steady-state power to both the telecommunications load 18 and to the auxiliary load 20'. The fuel cell stack 10' should therefore have a maximum power output capability of at least 1.4kW. If the fuel cell stack is taken off-line due to momentary fuel problems, etc., then the battery 14' should be able to provide the entire load. The battery would therefore also be sized to provide 1.4kW for the maximum expected period of fuel cell stack non-availability. Both of the power conditioners 12A' and 12B' should be sized to handle 1.4kW of power. The system therefore contains 2.8kW of power electronics (not including any power processing within the auxiliary or telecommunication loads).

Figure 3 shows another possible topology to accomplish the same task as the system in Figure 2. The system in Figure 3 employs 2 diodes to share power between the battery 14' and the fuel cell stack 10'. This topology may or may not reduce the cost of the power electronics depending on the required charging rate of the battery and the cost of the diodes. It also causes an unwanted side effect in that the diodes produce a significant loss of efficiency in the circuit.

A goal of the present invention is to provide an improved power conversion system that avoids the shortcomings of the approaches described above.

## SUMMARY OF THE INVENTION

In an exemplary embodiment of the present invention, a fuel cell or fuel cell stack is placed in parallel with a battery via a switch. The voltage on the output of the fuel cell, or stack, is held nearly constant by the battery and the power flow is controlled by adjusting the fuel cell operating parameters (such as temperature or air flow) and by opening and closing the switch. The result is a system that operates at nearly constant voltage without the need for an expensive power conditioning system. The output of the system can then be processed via a traditional power conditioning

system such as an inverter or dc-to-dc converter without the need for a wide range of input operating voltages. This reduces the cost and size of the fuel cell power conditioning system.

Although it is generally known that fuel cells and PV cells can be put in parallel with a battery to charge the battery, and that the output power conditioner can operate directly from the battery, the present invention is distinguished from the prior art by the regulation of the fuel cell to match the load. The prior art either slams the battery at high charge and discharge rates (thus causing shortened battery life) or it involves the use of a very large battery compared to load size. The latter is economically feasible only when there is a need to have many hours of back-up time.

Other aspects of the present invention are described below.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 schematically depicts one possible embodiment of a fuel cell-based power system exhibiting some of the problems addressed by the present invention.

Figure 2 depicts a more specific example of a fuel cell-based power system of the kind depicted in Figure 1. In this example, the load is a telecommunications system.

Figure 3 depicts a variation of the approach taken with the system of Figure 2.

Figure 4 illustrates a preferred embodiment of the present invention.

Figure 5 depicts voltage-current curves useful for explaining the operation of the inventive system of Figure 4.

#### DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

Figure 4 depicts a presently preferred embodiment of the invention. In this embodiment, a fuel cell stack 10' is placed directly in parallel with an energy storage device 14' (e.g., a battery or capacitor) through a switch  $S_1$ . The steady-state power flow from the fuel cell stack is controlled, using BOP controls (see BOP controller in Figure 4), by adjusting the fuel cell operating conditions such as temperature, air flow, fuel flow, air pressure or fuel pressure. The transient power flow comes from the storage device 14'. For example, when the load 18' suddenly increases, the energy storage device will provide power to meet the increase. The fuel cell operating conditions will then be adjusted to provide more power from the fuel cell stack 10'. As the fuel cell power increases, the output power from the energy storage device

decreases. When the load 18 suddenly decreases, the fuel cell stack 10' will be producing more power than required by the load. The extra power will flow into the battery until the fuel cell operating conditions allow the fuel cell to produce a lower output power.

5           This type of operation can be understood in more detail by examining the family of voltage-current (V-I) curves for the fuel cell stack 10' shown in Figure 5. When the fuel cell stack is placed in parallel with a battery, it is forced to operate at a fixed voltage. The current supplied by the fuel cell stack at this voltage will depend on the operating conditions of the stack. For example, based on the V-I curves shown in  
10   Figure 5, when the fuel cell is given operating condition op1, the current produced by the fuel cell stack would be 18A. Similarly, the current would be 9A with operating condition op2, or 5A with operating condition op3.

          In some cases, a battery will not be sized to accept a large charging current for an extended period. If this is the case, then when the output load significantly  
15   decreases, it may be necessary to open switch  $S_1$  for a short period of time until the fuel cell operating condition has been adjusted to match the decreased load. For the rare cases in which the battery cannot accept a large charging current for even the shortest period of time (e.g. – the time required to open mechanical switch  $S_1$ ), then an electronically switchable load (not shown) can be added in parallel with the battery  
20   to absorb the load transient while  $S_1$  opens. The electronically switchable load may also be used to reduce the number of open/close operations required of the mechanical switch, thus increasing the lifetime and reliability of the switch.

          The preferred embodiment of the invention allows the BOP to operate directly from the energy storage device without any efficiency penalties since the fuel cell  
25   stack can directly provide the auxiliary load. The efficiency of the auxiliary system is thus increased since there are no power electronics between the fuel cell stack and the auxiliary loads. Furthermore, the size of the power electronics has been substantially reduced from the system shown in Figure 2. The system shown in Figure 2 contains 2.8 kW of power electronics whereas the system shown in Figure 4 contains only 1  
30   kW of power electronics. It should be noted that the present invention is by no means limited to these power levels, i.e., the preferred embodiment may be employed to reduce the power rating of the power electronics by a ratio of 2.8/1, and other ratios may also be achieved. Furthermore, the conditioner shown in Figure 4 also only needs to operate from a small range of input voltages, thus simplifying the design of that

conditioner. The circuit of Figure 4 additionally removes the necessity of coordinating two power conditioners with each other, or coordinating any power conditioner with the fuel cell stack – instead, the dc-to-dc converter 12A'' of Figure 4 only needs to regulate the output voltage regardless of the fuel cell stack's operational status. The cost and complexity of the system is therefore much reduced from the system shown in Figure 2.

Persons skilled in the art of power generation will appreciate that the components described herein as making up the preferred embodiments of the present invention are well known and may be implemented in many different forms. Thus, the present invention is by no means limited to any particular form of fuel cell, battery, power conditioner, charger, or load. Moreover, it is apparent that the present invention may be practiced without necessarily using all of these components, or by replacing some or all of these with functional equivalents. For example, the power conditioner does not have to be present. Furthermore, some fuel cell systems may not require an auxiliary load. In some applications, the battery may be replaced with a capacitor, and the capacitor may be equipped with a low power circuit to help it maintain a nearly constant voltage. The switch connecting the fuel cell to the battery may be a mechanical switch, an electrical switch, or a combination of the two. The output of the power conditioner 12A'' and the load can be anything, DC, AC, or any voltage. The power conditioner is also not limited to any specific circuit topology. Moreover, the power and voltage levels are not limited to the levels mentioned above in connection with the presently preferred embodiment, although the fuel cell minimum operating voltage should be close to the battery float voltage in the case of the preferred embodiment. Accordingly, the scope of protection of the following claims is not intended to be limited to the presently preferred embodiments described herein.